

### **ME 1110 – Engineering Practice 1**

### **Engineering Drawing and Design - Lecture 16**

## Mechanical Elements Screws, Fasteners, non-permanent Joints

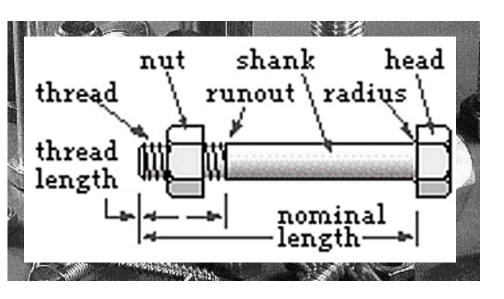
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www.staff.city.ac.uk/~ra600/intro.htm





### Introduction



The *helical-thread screw* was very important invention for application in:

- power transmission,
- angular to linear motion change,
- generation of large forces,
- non-permanent joints.

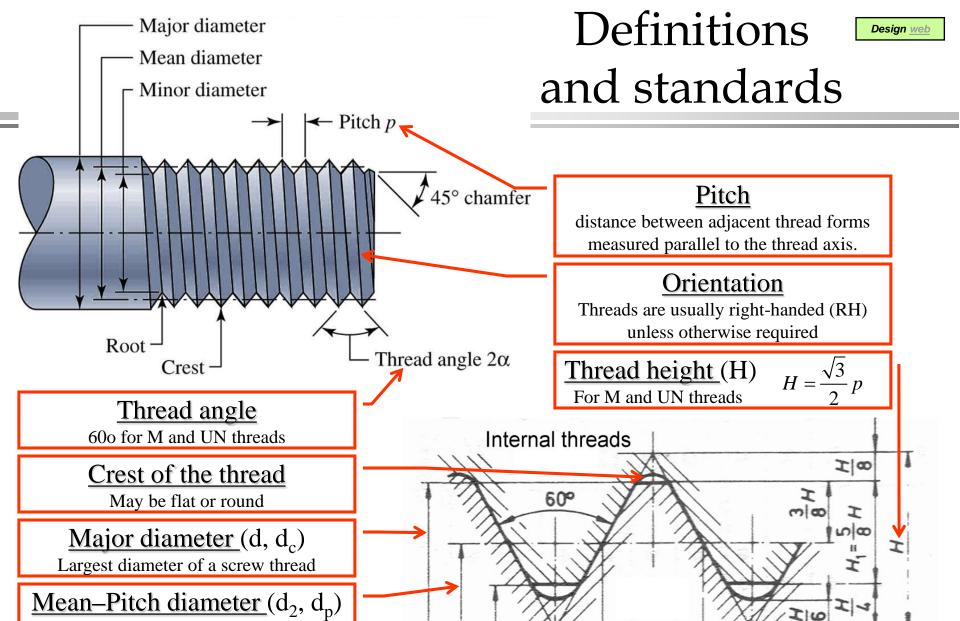
**Fastening**: the major target is to reduce number of joins. One of the most interesting subjects in engineering:

#### Example:

- Boeing 747 requires as many as 2.5 million fasteners. Some are very expensive.

Designer's *aim is to select an adequate fastener* (bolt, nut, cap, screw ...) for an application in question: - the shape and the arrangement

- the size and other functional parameters
- to check if selected fastener can sustain required load



External threads

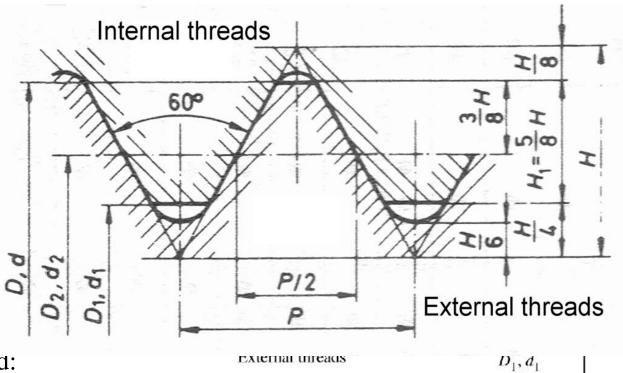
Mean diameter; teeth section is p/2 long

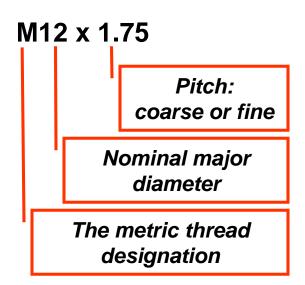
 $\frac{\text{Minor diameter}}{\text{Smalest diameter of the thread}} (d_1, d_r)$ 

# CIScrew Threads

#### **Metric Threads**:

- Thread angle =  $60^{\circ}$
- Symmetric profiles
- Identified as M and MJ
- Coarse and fine pitch
- Specification of the thread:







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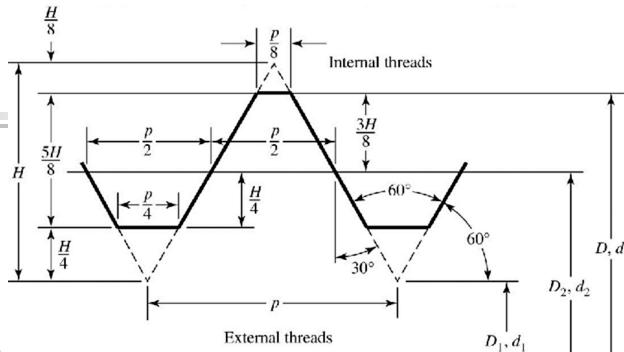
EST 1894

Nominal	C	oarse-Pitch	Series	Fine-Pitch Series				
Major Diameter <i>d</i>	Pitch	Tensile- Stress Area <i>A</i> ,	Minor- Diameter Area A,	Pitch	Tensile- Stress Area <i>A</i> ,	Minor- Diameter Area A <sub>r</sub>		
1.6	0.35	1.27	1.07	7	/	•		
2	0.40	2.07	1.79	- 5 -	Metı	$^{\prime}1C$		
2.5	0.45	3.39	2.98	, <del></del>	<b>VIC 61</b>	- 45		
3	0.5	5.03	4.47	. 1		1		
3.5	0.6	6.78	6.00	T I	nrea	<b>OS</b>		
4	0.7	8.78	7.75					
5	0.8	14.2	12.7	(all di	mension	s in mm)		
6	1	20.1	17.9					
8	1.25	36.6	32.8	1	39.2	36.0		
10	1.5	58.0	52.3	1.25	61.2	56.3		
12	1.75	84.3	76.3	1.25	92.1	86.0		
14	2	115	104	1.5	125	116		
16	2	157	144	1.5	167	157		
20	2.5	245	225	1.5	272	259		
24	3	353	324	2	384	365		
30	3.5	561	519	2	621	596		
36	4	817	759	2	915	884		
42	4.5	1120	1050	2	1260	1230		
48	5	1470	1380	2	1670	1630		
56	5.5	2030	1910	2	2300	2250		
64	6	2680	2520	2	3030	2980		
72	6	3460	3280	2	3860	3800		
80	6	4340	4140	1.5	4850	4800		
90	6	5590	5360	2	6100	6020		
100	6	6990	6740	2	7560	7470		
110		Son alle on		2	9180	9080		

# Screw Threads

#### **Metric Threads**:

- Thread angle =  $60^{\circ}$
- Symmetric profiles
- Identified as M and MJ
- Coarse and fine pitch
- Specification of the thread:



#### M12 x 1.75

Pitch: coarse or fine

Nominal major diameter

The metric thread designation

Thread series: UNC, UNF, UNRC, UNRF

Threads per inch (coarse or fine)

Nominal major diameter

#### **Unified threads:**

(usually pipe threads)

Thread angle =  $60^{\circ}$ 

- Symmetric profiles
- Serief UN and UNR
- Coarse (C) and fine (F) pitch
- Specification of the thread:

#### 1/4 in-20 UNRC



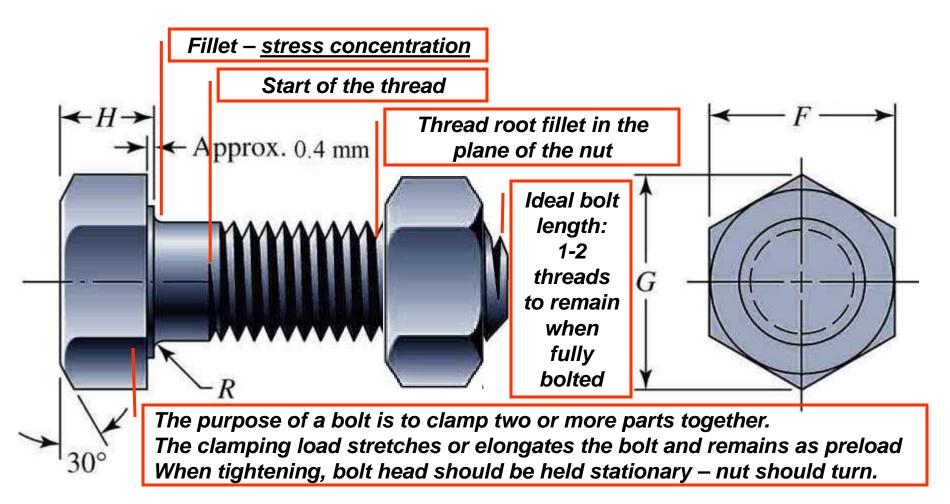


### Unified Screw Threads (dimensions in ")

A 18 (18 18)		Co	arse Series—	-UNC	Fine Series—UNF				
Size Designation	Nominal Major Diameter in	Threads per Inch N	Tensile- Stress Area A, in <sup>2</sup>	Minor- Diameter Area A, in <sup>2</sup>	Threads per Inch N	Tensile- Stress Area A, in <sup>2</sup>	Minor- Diameter Area A, in <sup>2</sup>		
0	0.0600		tower 1 to	ech anics s	80	0.001 80	0.001 51		
rotion islanding	0.0730	64	0.002 63	0.002 18	72	0.002 78	0.002 37		
pewer 2 hear of	0.0860	56	0.003 70	0.003 10	64	0.003 94	0.003 39		
3	0.0990	48	0.004 87	0.004 06	56	0.005 23	0.004 51		
4	0.1120	40	0.006 04	0.004 96	48	0.006 61	0.005 66		
5	0.1250	40	0.007 96	0.006 72	44	0.008 80	0.007 16		
6	0.1380	32	0.009 09	0.007 45	40	0.010 15	0.008 74		
8	0.1640	32	0.0140	0.011 96	36	0.01474	0.012 85		
10	0.1900	24	0.017 5	0.014 50	32	0.020 0	0.017 5		
12	0.2160	24	0.024 2	0.020 6	28	0.025 8	0.022 6		
$\frac{1}{4}$	0.2500	20	0.031 8	0.026 9	28	0.036 4	0.032 6		
1/4 5/16	0.3125	18	0.052 4	0.045 4	24	0.058 0	0.052 4		
	0.3750	16	0.077 5	0.067 8	24	0.087 8	0.080 9		
3 8 7 16	0.4375	14	0.1063	0.093 3	20	0.1187	0.1090		
	0.5000	13	0.141 9	0.1257	20	0.159 9	0.148 6		
$\frac{\frac{1}{2}}{\frac{9}{16}}$	0.5625	12	0.182	0.162	18	0.203	0.189		
	0.6250	11	0.226	0.202	18	0.256	0.240		
3/4	0.7500	10	0.334	0.302	16	0.373	0.351		
5 8 3 4 7 8	0.8750	9	0.462	0.419	14	0.509	0.480		
1	1.0000	8	0.606	0.551	12	0.663	0.625		
1 1/4	1.2500	7	0.969	0.890	12	1.073	1.024		
$1\frac{1}{2}$	1.5000	6	1.405	1.294	12	1.581	1.521		



### **Threaded Fasteners**



Hexagon head bolt

8



## Properties of a threaded fastener

The *shank* diameter of a 'waisted' bolt is less than the thread diameter; allows a thread run out which reduces stress concentration.

A *Washer* under the nut ensures uniformity of a contact.

A bolt's '*grip*' is the combined thickness of the fastened parts

**Bolt** - has a nut which turns to tighten

**Screw** - turns itself in the threaded hole

**Stud** - has no head and is threaded on both sides

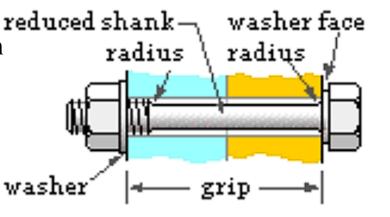
*Clearance hole* - 15-20% larger than a bolt/stud size

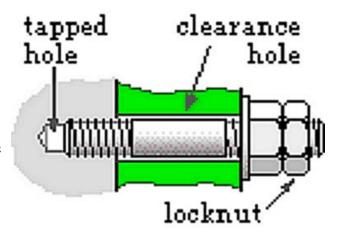
**Taped hole** - drilled smaller than the *minor* dia.

extends deeper than the stud

**Stud depth** - 1.5 times the major diameter

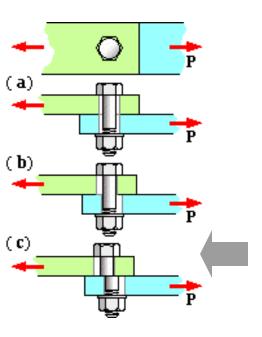
**Thread length** - only a couple of threads longer than a bolt







### Load that a bolt can sustain





$$\sigma = \frac{F_b}{A_t}$$

**Shear stress:** 

$$\tau = P/A_r$$

exposed threads	y pitch	section X-X through exposed threads
	nut X	minor Miameter Major stress area

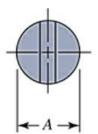
	_	_					
	class no.	4.6	5.8	8.8	9.8	10.9	12.9
St	Tensile [Mpa]	400	500	800	900	1000	1200
Sy	Yield [Mpa]	240	400	640	720	900	1080
Sp	Proof [Mpa]	225	380	590	650	830	970
	Elongation %	22	20	12	10	9	8

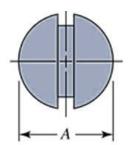
Strength table

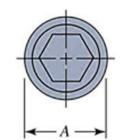


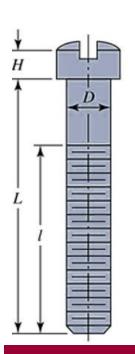


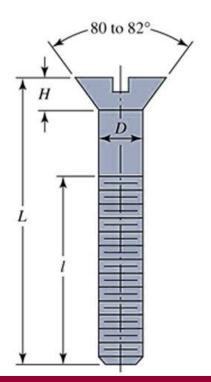
# Typical cap-screw heads

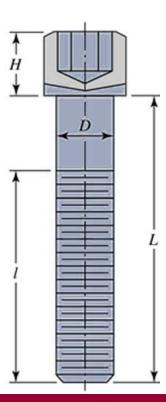












Fillister head

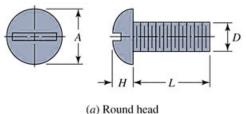
Flat head

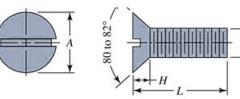
**Hexagonal socket head** 

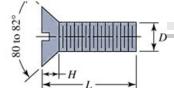




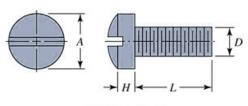
### Other types of screw heads in use

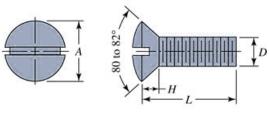


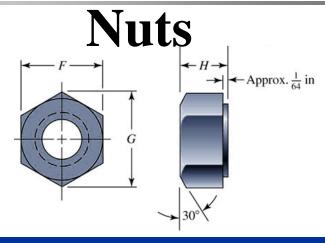




(b) Flat head



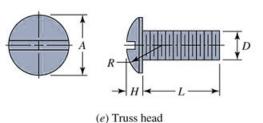


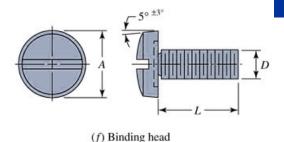


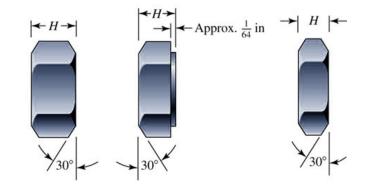
(c) Fillister head

(d) Oval head

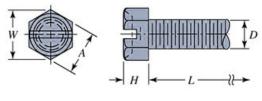
#### Hexagonal washer faced regular nut





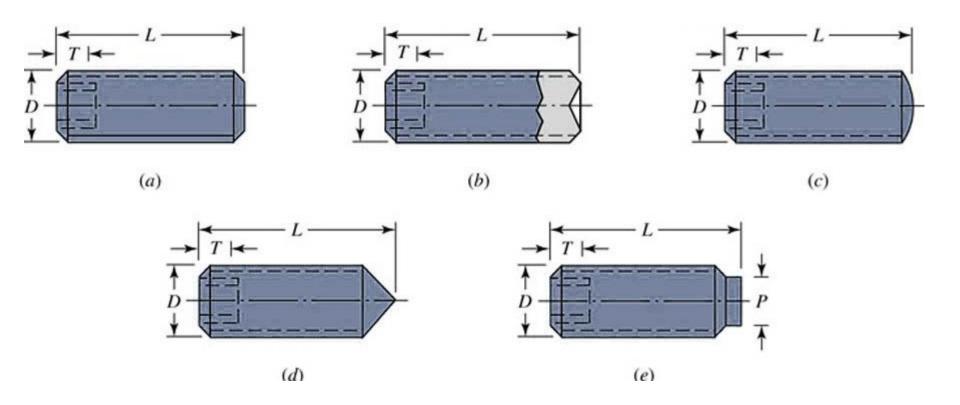


(g) Hex head (trimmed)



regular nut chamfered on both sides jam nut with washer face jam nut chamfered on both sides (h) Hex head (upset)

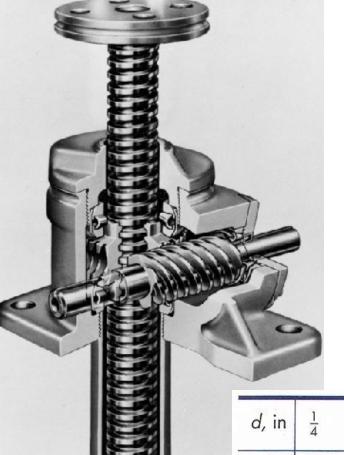
# **Setscrews**

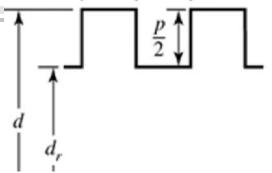


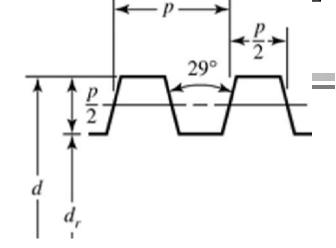
regular nut chamfered on both sides jam nut with washer face jam nut chamfered on both sides



### Threads for power screws







Design well

#### **Square and Acme threads:**

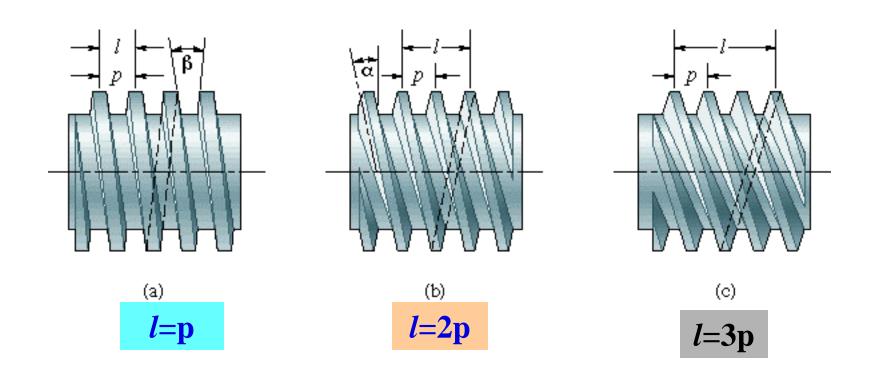
- Used for power transmission
- These have preferred sizes but also can vary
- Modifications to these threads are easy

#### **Preferred Pitches for power threads:**

d, in	1/4	<u>5</u>	3/8	1/2	<u>5</u> 8	3/4	<u>7</u>	1	$1\frac{1}{4}$	$1\frac{1}{2}$	1 3/4	2	$2\frac{1}{2}$	3
p, in	1/16	1/4	1/12	10	1/8	16	1/6	1/5	1/5	1/4	1/4	1/4	1/3	1/2

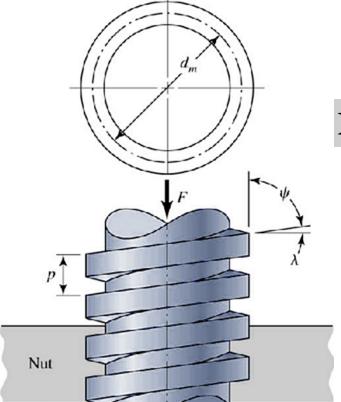


# Multiple threaded screws



(a) Single, (b) double, (c) triple threaded screws.





### **Power screws**

### Rising the load

$$\sum_{x} F_{x} = P_{R} - N \sin \lambda - f N \cos \lambda$$

$$\sum F_{y} = F + f N \sin \lambda - N \cos \lambda$$

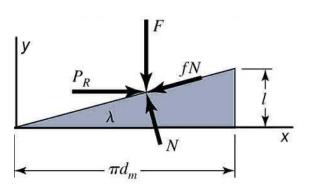
$$P_{R} = \frac{F(f\cos\lambda + \sin\lambda)}{\cos\lambda - f\sin\lambda} \qquad T_{R} = \frac{Fd_{m}}{2} \left(\frac{\pi f d_{m} + 1}{\pi d_{m} - f l}\right)$$

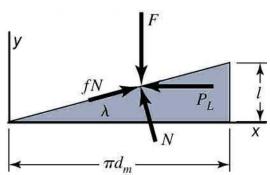
$$T_{R} = \frac{Fd_{m}}{2} \left( \frac{\pi f d_{m} + 1}{\pi d_{m} - f l} \right)$$

### Lowering the load

$$\sum F_{x} = -P_{L} - N \sin \lambda + f N \cos \lambda$$

$$\sum F_{y} = F - f N \sin \lambda - N \cos \lambda$$





$$P_{L} = \frac{F(f\cos\lambda - \sin\lambda)}{\cos\lambda + f\sin\lambda}$$

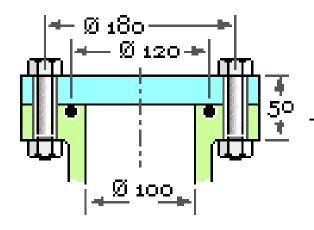
$$T_{L} = \frac{Fd_{m}}{2} \left( \frac{\pi f d_{m} - 1}{\pi d_{m} + f l} \right)$$

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# Example



The cover of a pressurised cylinder is attached by a self-energising seal and 6 identical bolts M10x1.5 of class 8.8. The fluid pressure is essentially constant at 6 MPa. A safety factor of three is required. Check if the given bolt can sustain the pressure!

6 class 8.8 M10x1.5

$$d_s=120 \text{ mm} N_d=3$$

$$N_d = 3$$

$$S_t/\sigma=?$$

#### **SOLUTION:**

Force on the cover caused by the pressure:

$$F_c = p \cdot A_s = p \frac{\pi d_s^2}{4}$$

$$F_c = p \cdot A_s = p \frac{\pi d_s^2}{4} \qquad F_c = 6 \cdot 10^6 \frac{\pi \cdot 0.12^2}{4} = 67858N = 67.9kN$$

$$F_b = \frac{F_c}{6} = 67.9 \frac{6}{6} \qquad F_b = 11.3kN$$

Force on the individual bolt

$$F_b = \frac{F_c}{6} = 67.9$$

Proof strength  $S_p = 590 MPa$ 

From tables:

Tensile stress area  $A_{c} = 58mm^{2}$ 

$$\sigma = \frac{F_b}{A} = \frac{11300}{58} \qquad \sigma = 194MPa$$

Stress on each bolt:

$$\frac{S_p}{\sigma} = \frac{590}{194} = 3.04 \approx N_d$$